Equilibrium and Kinetics studies for Removal of Heavy Metals from simulated Wastewater using Chitosan/Activated carbon composite

Ahmed Saad Ali a, Ali Mustafa A. Hassan b, Mohammed Hamdi Nour c

Abstract

Removal of lead, copper, and cadmium from aqueous solution with chitosan/activated carbon (CH/AC) composite was studied under batch equilibrium technique setup. The composite was prepared by blending chitosan gel with activated carbon by ratio of (3:1). The physical and chemical characters of the composite was studied by several analyses; (bulk density, BET surface area, pHpzc, SEM, and EDX). The adsorption behavior of the target metals was examined as function of pH, contact time, sorbent dose, and initial metal concentration. Prior to the batch equilibrium experiments the metal hydroxide precipitation was studied to determine the pH edge of the metal precipitation. The lead hydroxide precipitation edge is ≥ 6.0 while the copper and cadmium hydroxide precipitation is ≥ 7.0. pHpzc experiment revealed positive surface charge of the composite at pH equal to 7.6 that means electrostatic attraction is not the dominant mechanism for the sorption of cations. The optimum pH was 5.5, 6.0 for lead and both copper and cadmium respectively. qe was 13.1 mg/g, 12.2 mg/g, and 10.4 mg/g for copper, lead, and cadmium respectively. Adsorption isotherms for the three metals is correlated well with Langmuir type of adsorption isotherm which means that chemisorption is the dominate mechanism in the sorption process. Also, the adsorption process for the three metals were found to follow pseudo second order type of adsorption kinetics, which revealed that the rate-limiting factor might be chemisorption involving valance forces through sharing of electrons between the amino groups of chitosan and the metal ions.

Keywords: Adsorption; Heavy *Metals, Chitosan*; composite; Isotherm; Kinetic

1. Introduction

^a Environmental Engineering Program, School of Science and Engineering, The American University in Cairo, P.O. Box 74, New Cairo 11835, Egypt. (Corresponding author e-mail: asaad@aucegypt.edu).

^b Chemistry Department, Faculty of Science, Al-Azhar University, Nasr City 11884, Cairo, Egypt

^c Civil Engineering Department, Faculty of Engineering, Cairo University, Giza, Egypt

The direct or indirect discharge of heavy metals into aquatic systems has become a matter of concern in the world over the last few decades. They have been prioritized as major inorganic contaminants in the environment because of their accumulation tendency, hazardous effect, and toxicity to the human life and environmental health [1]. Unlike the organic contaminants where the majority of which are susceptible to biological degradation into harmless end products, heavy metals are not biodegradable and tend to accumulate in living organisms causing numerous diseases and disorders [2]. The term heavy metals refers to the elements that have atomic weights between 63.5 and 200.6, and density greater than 5.0 gm/cm³ (e.g. Ag, Hg, Pb, Cr, Cd, As, Al, Cu ...) [3,4]. Lead, cadmium and copper are the most common toxic heavy metals in the industrial wastewater effluents [5]. The potential sources of these heavy metals in wastewater are discharge waste stream from electric batteries manufacturing, nickel/cadmium batteries, lead smelting, plumbing, glass industry, gasoline additive, ceramic and porcelain enameling, piping, electroplating, and oil/gas exploration and drilling [6-8]. The World Health Organization (WHO) guidelines values of lead, copper, and cadmium in drinking water are 0.01, 2.0, and 0.003 mg/L respectively [9]. Several remediation techniques have been employed to mitigate or remove heavy metals from wastewater. The commonly used techniques are chemical precipitation, coagulation-flocculation, phytoremediation, reverse osmosis, exchange, carbon adsorption, resin sorption, electro-dialysis, and adsorption [10-11]. However, most of these technologies are not eco-friendly or economically viable and have significant demerits such as hazardous sludge formation which convert the aquatic problem into solid problem, incomplete metal removal, and high cost at large scale [12-13]. Motivated by cost consideration, the efficiency of low cost adsorbents like agricultural wastes and seafood processing wastes is the promising alternative. Recently, a considerable attention has been focused on the biosorbents (sorbent materials with biological origin) as an efficient, low cost,

and eco-friendly materials for the treatment of wastewater containing heavy metals [14]. One of such kinds is chitosan, β -(1 \rightarrow 4)-linked -Dglucosamine units (deacetylated units) together with some proportion of N-acetyl -Dglucosamine units (acetylated units), which can be produced from fishery waste by partially alkaline deacetylation of Chitin. Chitin, β -(1 \rightarrow 4)linked-N-acetyl-D-glucosamine, is the second most abundant biopolymer next to cellulose, can be extracted commercially from the shells of crustacean (such as crabs, shrimps, prawns, krill), insects, and fungi [15-16]. Chitosan and its derivatives have been applied in different fields from pharmaceutical, ranging medicine, cosmetics to wastewater and drinking water treatment. [17-18]. Chitosan is more useful and effective biosorbent as compared to chitin, since it has unique and distinctive features like, biodegradability, nontoxicity, high reactivity, excellent chelation behavior due to the presence of amine and hydroxyl functional groups which show high adsorption potential for various aquatic pollutions, and low cost in comparison with other adsorbents. However, it cannot be used in the raw form due to the presence of undesirable characters such as low mechanical strength and poor chemical resistance like swelling and solubility in acidic solutions. Physical and chemical modifications methods have been used to modify raw chitosan. These methods include crosslinking, grafting, and blending. The modifications were proposed in order to improve pore size, mechanical strength, chemical stability, and hydrophilicity [19]. Recently, chitosan blending has become one of the effective methods for providing new desirable polymeric materials for practical applications. Different kinds of substances have been used in blending with chitosan to form composite such as activated clay, polyurethane, cotton fibers, magnetite, cellulose, perlite, ceramic alumina, calcium alginate, sand, polyvinyl chloride (PVC), polyvinyl alcohol (PVA), and activated carbon [20]. As the activated carbon has unique porous structure, high specific surface area and high mechanical and chemical resistance which will offer desirable properties to

chitosan by blending with it in composite. Moreover it can be prepared from non-expensive sources such as agriculture wastes; (e.g. cotton stalks, rice straw, coconut shells, sugar can bagasse, etc.....)[21]. The polymeric composite; chitosan/activated carbon (CH/AC) represents one of the environmental friendly solution by transforming the materials with negative value to valuable materials. This work aims to investigate the influence of various experimental parameters (pH, contact time, sorbent dose, and initial metal concentration) on the sorption of lead, copper, and cadmium by CH/AC composite as a potential and low cost sorbent. Moreover, the experimental results were evaluated using both Langmuir and Freundlich isotherm models and pseudo first order and pseudo second order kinetic models to obtain the needed parameters. To get results with good level of confidence all experiments were conducted twice and mean values were used

2. Material and Methods

2.1. Material

Practical grade chitosan flakes (CH) with degree of de-acetylation ≥ 75%, and molecular weight of 190-375 kilo Dalton (KDa) was purchased from Sigma-Aldrich Company. Commercial activated carbon (AC) granular shape was purchased from the local market. Stock solutions of (1000 mg/L) Lead, copper, and cadmium, were purchased from MERCK Company. Deionized distilled water (DDW) was used in the preparation of all the solutions and standards in the experiments and the analyses. NaNO₃ salt (assay 99%) manufactured by (GCC) company, United Kingdom, was used as ionic background in the metals solutions. Concentrated nitric acid and Sodium hydroxide pellets with American Chemicals Society (ACS) grade, were purchased from MERCK Company. Acetic acid with concentration 96%, with ACS grade was purchased from Free Trade Egypt Company.

2.2. Preparation of CH/AC composite

CH/AC composite with ratio of 3:1 (CH.: AC.) was prepared according to (Hakimeh Sh. *Et.al.* (2012), Viorica P.; *et.al.* (2013), Xiaoyu Ch., and Lindun

He, (2017)) [22-24] with slight modification, as the following. A 30.0 grams' amount of commercial (CH.) flakes was dissolved in 500 ml of 5% (v/v) acetic acid solution under continuous stirring at 45-50°C until formation of (CH) gel. About 10 grams of granular (AC) was added slowly to the (CH) gel and stirred for 24 hours at 45-50°C. Then, the (CH/AC) composite beads were prepared by injecting the (CH/AC) gel in droplets through a syringe nozzle into a 500 ml of 0.1 M NaOH precipitation bath. The composite beads were allowed to stay in the NaOH precipitation bath with slow stirring for 6 hours. After that, the beads were separated from NaOH solution by filtration, and washed several times with deionized water to a slightly neutral pH (7.5 ± 0.5). Finally, the beads were dried in air oven at 60°C for 24 hours, and grinded. After that, the materials were sieved, passed through Mesh No. 25 (0.7 mm) and collected on Mesh No. 35 (0.5 mm). The homogenous particles with particle sizes of (0.5-0.6) mm were dried and kept in desiccator prior to work.

2.3. Characterization of CH/AC composite

The composite was characterized by the selected physical and chemical analyses:

Bulk density:

To measure bulk density, a pre-weighted 10 ml cylinder was filled to a specified volume with dried adsorbent; (the dry material was freely settled). Then the cylinder was weighted with the dry material, and the weight of the dry material was calculated as:

Weight of dry material (g) = weight of the cylinder with the material - weight of the empty cylinder [1]

The bulk density calculated as [25]:

weight of the dry material (g) volume of the dry metrial (cm3)

•BET surface area:

It was determined from adsorption-desorption isotherm of nitrogen gas at 77K, by using a

Micrometrics —ASAP 2020 surface area and porosity analyzer. Prior to the analysis, the samples were degassed at 60 °C for 4 hours under a vacuum of 10 um Hg. The specific surface area was calculated using Brunauer — Emmett- Teller (BET) method, while pore volumes and average pore diameter were calculated by the Barrett-Joyner- Halenda (BJH) method.

• pH point of zero charge (pHpzc):

 (pH_{nzc}) is often used to study the impact of the electrostatic surface charge of the adsorbent on the adsorption process. It is the pH value at which the surface charge of the material becomes equal to zero under given conditions of temperature, applied pressure, and aqueous solution. This does not mean that the surface has no charge at (pHpzc), but rather that there are equal amounts of positive and negative charges on the surface [26]. The experiment was done by salt addition method [27] as the following: ten samples of each material with 0.1 g each were added into ten 125 ml high density polyethylene (HDPE) bottles. Then, a portion of 50 ml 0.01M purged sodium nitrate solution was added to each bottle. After that, pH of the solutions was adjusted to the desired pH values (from 2 to 11) using 0.1 M NaOH or 0.1 M HNO3 and recorded as initial pH (pH_I). After 48 hours of continuous shaking on rotary shaker, with speed of 150 round per minute (rpm), the solutions were filtered, through 0.45 um cellulose nitrate membranes in plastic filtering device. The pH of each filtrate was measured and recorded as final pH (pH_F). The difference between initial pH and final pH was calculated and reported as Δ pH.

$\Delta pH = final pH (pH_F) - initial pH (pH_I)$ (3)

The (pHpzc) would be determined by plotting Δ pH against initial pH (pH_I). It is the point at which the curve of Δ pH crosses the line of initial pH (pH_I)

SEM & EDX analysis:

The surface morphology of the composite before and after metals sorption was conducted by the Scanning Electron Microscope; SEM (model LEO SUPRA 55, manufactured by ZEISS company, Germany). While the elemental

analysis of the composite before and after metals sorption was conducted by the Energy Dispersive X-ray; EDX unit which represents a complementary technology to the SEM. The Samples were coated by thin layer of gold prior to the analysis to be more conductor.

2.4. Batch equilibrium experiments

The sorption isotherm is the ratio between the quantity adsorbed and the quantity remaining in solution under fixed temperature at equilibrium [28]. The optimum environmental factors such as initial pH, contact time, initial composite dose, and initial metal concentration are studied in this set experiments. These factors are known with their significant effect on the sorption equilibrium. The purpose of these experiments is to determine the optimum pH, the time of equilibrium, and the sorption capacity of the composite. The batch experiments are carried out in well-sealed 125 ml high density polyethylene (HDPE) bottles. When these bottles agitated, they can be assumed to function as completely mixed batch reactors. The volume of each sample in the experiments was 50ml of synthetic wastewater solution containing 30 mg/L from the target metal and 0.1M NaNO₃ as ionic background to simulate the effect of the anions and the cations in the real wastewater. The desired pH of the samples was adjusted by 0.1MNaOH or 0.1 MHNO₃. The composite was added to all the samples except the control samples. The samples were shaked at room temperature (22.0±0.5 °C) on the rotary shaker at 150 round per minute (r.p.m). The experiments were carried out under controlled pH. Subsequently, each sample was filtered through prewashed cellulose acetate filter paper (0.45 um), and acidified to pH<2.0 using 1:1 HNO3 and analyzed by Atomic Absorption Spectrometer (AAS) model Sence AA. The percentage removal (% R) of each metal was calculated using the

Equation:
$$\%$$
 removal = $\frac{Ci-Cf}{Ci}$ x 100 (4)

The sorption capacity is obtained by using the mass balance equation:

$$qt = \frac{Ci - Ct}{m} \times V$$
 (5)

$$q_e = \frac{Ci - Cf}{m} \times V \tag{6}$$

Where, q_t and q_e are the amounts of metal ions adsorbed at time t and at equilibrium respectively in mg of metal per g of sorbent (mg/g), C_i and C_f are the initial and final metal ion concentration in (mg/L), C_t is the concentration of metal ions at time t, V is the volume of the solution in (L) , and m is the weight of dry sorbent (composite) (g).

•Metal Hydroxide Precipitation experiment:

The experiment was conducted to investigate the metal hydroxide precipitation as function of pH. It was carried out at pH range (2-11). Each sample contains 30 mg/L from each target metal individually without composite.

• Effect of pH experiment:

Based on the previous experiment of metal hydroxide precipitation, the experiment was carried out at controlled pH ranges (2.0-6.0 \pm 0.05) for Pb(II) and (2.0-7.0 \pm 0.05) for both Cu(II) and Cd(II). The samples were shaked for about 5 hours.

• Effect of contact time experiment:

This experiment was carried out at time range (0-600) minutes, at the optimum pH for each target metal; (5.5 \pm 0.05) for Pb(II), and 6.0 \pm 0.05 for Cu(II), and Cd (II).

• Effect of composite dose experiment:

The experiment was conducted with composite doses of (0.5-4.5) g/L at the optimum conditions.

Effect of initial metal concentration

The experiment was conducted with metal concentrations of (10-200) mg/L from each target metal.

2.5. Sorption isotherm models

•Langmuir isotherm model:

The Langmuir isotherm (1918) is an empirical model assumes homogenous sorption sites and sorption energies on the surface of adsorbents. Also, it assumes that, there is not any interaction between the adsorbed molecules (i.e. the ability of molecule to adsorb at a given site is independent on the occupation of the neighboring sites [29]. The linear form of the model is presented by the equation:

$$\frac{1}{q_e} = \frac{1}{C_e q_m b} + \frac{1}{q_m} \tag{7}$$

Where, q_e (mg/g) is the amount of adsorbate adsorbed per gram of adsorbent at equilibrium (adsorption capacity). C_e (mg/L) is the equilibrium (residual) concentration of the metal ions in the solution, q_m (mg/gm) is the maximum (ultimate) adsorption capacity, and b (liter/mg) is the Langmuir constant related to the binding energy of adsorption. Plotting of $\frac{1}{q_e}$ versus $\frac{1}{c_e}$ would give the Langmuir constants q_m and b. The higher the value of b the higher the affinity of the sorbent to the sorbate.

• Freundlich Isotherm model:

The Freundlich isotherm model is based on the heterogeneity. It assumes that the sorption sites have heterogeneous energy, varied strength, and work in multi-layer [30]. The linear form of the model is presented by the equation:

$$\log q_e = \log K_F + \frac{1}{n} \log C_e \tag{8}$$

Where, q_e (mg/g) is the mass of metal adsorbed per gram of adsorbent at equilibrium; (adsorption capacity), C_e (mg/liter) is the equilibrium of metal concentration in the solution, K_F and 1/n are Freundlich isotherm constants (empirical constants). They are indicator of adsorption capacity, and adsorption intensity respectively. The smaller the value of $\frac{1}{n}$ the stronger the adsorption bonds. These constants can be obtained by plotting $\log q_e$ versus $\log C_e$

2.6. Kinetic models

In order to investigate the controlling mechanism of the sorption processes, the

sorption rate constants, and sorption capacity, pseudo first-order and pseudo-second order kinetics were applied in the data of adsorption.

•Pseudo First - Order Kinetic

The pseudo first-order kinetics can be expressed as: Log $(q_e - q_t) = \log q_e - \frac{K1}{2.303} t$ (9)

Where, K_1 is the rate constant of pseudo first – order adsorption (min⁻¹); q_e and q_t are the amount of metal ion adsorbed per gram adsorbate at equilibrium and at any time t respectively (mg/g). Plotting of Log ($\mathbf{q_e} - \mathbf{q_t}$) versus t would give the first – order rate constant K_1 and equilibrium adsorption capacity q_e from the slope and intercept of the straight line .

•Pseudo Second - Order Kinetic

The pseudo second – order kinetics can be expressed as: $\frac{t}{q_t} = \frac{1}{\kappa_2 q_t^2} + \frac{t}{q_t}$ (10)

Where K_2 (g / mg min) is the rate constant of pseudo second-order kinetic model. Plotting of t/q_t versus t would give the pseudo second – order rate constant K_2 and q_e .

3. Results and Discussion

3.1. Characteristics Analysis.

The bulk density, surface area, pore volume, and pore size of the composite, CH, and AC are shown in Table 1. It has shown that improvement in the composite properties in comparison with CH. Significant increase in surface area and pore volume of the composite is related to blending of it with AC. Obviously the metal uptake capacity of the composite will be higher due to the presence of more free adsorption sites. Bulk density of the adsorbent material has an effect on its adsorption efficiency and the performance of the adsorption process [31]. The moderate value of Bulk density of the composite in comparison with CH and AC gives it desirable character in adsorption efficiency and adsorption performance in the treatment plants. The average pore diameter of the composite particles indicates that, the material of the composite is mesoporous material, according to International

Union of pure and applied Chemistry (IUPAC) classification, among different porous materials, mesoporous material is most favorable in aqueous system, as they have moderate diffusion flux and highly efficient mass transfer are achievable due to their appropriate pore dimension, high specific surface area and good organic adsorption capacity [32]. - In order to understand the sorption mechanism, it is necessary to determine the zero charge point (pHpzc) of the adsorbent material as it indicates how easily the adsorptive materials are able to adsorb the ions of target pollutants [33]. The pHpzc value of composite is about 7.6; (higher than the optimum pH value of Pb (II), Cu (II), and Cd (II), as shown in the next part of study). This

Table 1: Physical characteristics of CH/AC composite, commercial CH, and AC.

Parameter	composite	CH.	AC.
Bulk density (g/cm³)	0.32	0.198	0.5007
рНрzс	7.6	5.95	8.36
BET surface area (m²/g)	287.352	0.543	773.7
Total pore volume (cm3/g)	0.160	0.001	0.417
Average pore diameter (nm)	2.232	10.97	2.156

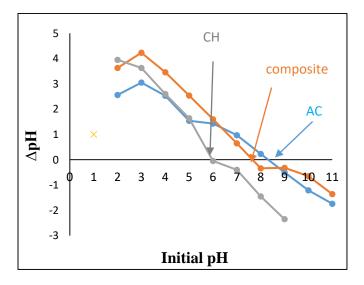


Figure 1: pH point of zero charge (pHpzc) of composite, CH, and AC.

revealed that the electrostatic interaction (physisorption) between the metal ions M⁺ and the surface of the composite could be hard, and other mechanism (chemisorption) could be work as a dominant mechanism between M⁺ ions and the active groups on the composite surface.

SEM & EDX analysis

Figures 2 and 3 displays the presence of pores and cracks on the surface of composite confirming the higher surface area of it, while the surface of chitosan has relative smooth structure confirming its low pore volume and surface area.



Figure 2: SEM micrographs of chitosan

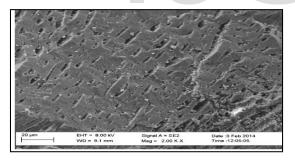


Figure 3: SEM micrographs of composite Table2: EDX analysis of raw composite

Tablez. LDX analysis of raw composite				
Element	Wt.%	At. %		
NK	8.34	10.38		
ОК	73.94	80.54		
Al K	9.93	6.42		
Ca K	5.26	2.29		
Fe K	0.72	0.22		
Au M	1.81	0.16		
Totals	100			

Table3: EDX analysis of composite after Pb (II) sorption

Element	Wt.%	At. %
N K	2.70	7.35
O K	32.76	77.62
Al K	1.83	2.57
Ca K	1.25	1.18
Fe K	-	-
Pb M	58.34	10.67
Au M	3.1	0.30
Totals	100.0	

Table4: EDX analysis of composite after Cu (II) sorption

Element	Wt.%	At. %
NK	5.89	9.1
ОК	58.99	79.82
Al K	-	-
Ca K	3.61	1.96
Fe K	-	-
Cu K	24.51	8.35
Au M	6.98	0.77
Totals	100	

Table 5 EDX analysis of composite after Cd (II) sorption

Element	Wt. %	At. %
NK	15.9	18.78
ОК	59.39	61.43
Al K	0.6	0.37
Ca K	2.72	1.12
Fe K	-	-
Cd L	9.09	1.34
Au M	12.31	16.96
Totals	100	

- The EDX analysis of the composite before and after metals sorption is shown in Table 2,3,4,5 respectively. It showed significant change in the nitrogen and oxygen composition of the composite after metals sorption. It revealed the role of active amine groups of CH and active hydroxyl groups of both CH and AC in the sorption process of the three metals by the composite. This means that, chelation of metal ions by the active groups of the composite is one of the possible mechanisms. Moreover, the decrease or

disappearing of Al, Ca, and Fe after metals sorption explains that the ion exchange mechanism could be one of the possible mechanisms with small value.

3.2. Batch equilibrium studies

3.2.1. Metal hydroxide precipitation

Figure 4 concludes that drastic change in lead precipitation started at pH value of 6.0 with ratio of 20% to reach to 67% at pH 7.0. So that, precipitation is considered the dominant mechanism of lead removal at pH \geq 6.0. This observation has been also confirmed by other authors (Venkatesham et.al., 2013 [34], and Cechinel et.al., 2014 [35]. While for copper the precipitation started at pH 6.5 with ratio of 30% to reach to 46% at pH 7. And for cadmium the precipitation started at pH 7 with ratio of 12% to reach to 53% at pH 8. Based on the results of this experiment, and to ensure solubility of the metals to eliminate the consequence of metal precipitation, the following experiment (effect of initial pH) was carried out at pH values of (2.0-6.0) for lead, and (2.0-7.0) for both copper and cadmium.

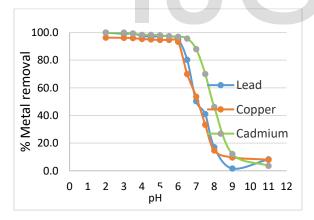


Figure 4: Pb⁺², Cu⁺², and Cd⁺² hydroxides precipitation as function of pH

3.2.2. Effect of pH

Sorption of metal ions from aqueous solution is related to the pH of the solution, as the later affects the degree of ionization of the metal and the surface charge of the sorbent (pH_{zcp}) [36]. Figure 5 shows that CH/AC composite has significantly lower sorption capacity for metal

uptake at pH below 3. This is due to that, at low pH the amine groups of the chitosan in the composite get protonated. That means surface of the composite will get positive charg, and a force of repulsion will occur between the metals (Pb⁺², Cu⁺², Cd⁺²) which have positive charge and the active sites instead of attraction.

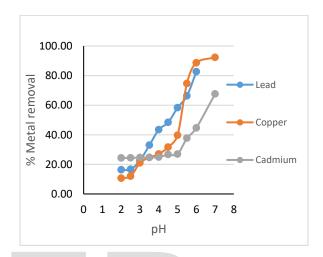


Figure 5: Effect of pH on sorption of 30 mg/L heavy metals using 2g/L CH/AC composite - % removal.

Moreover, at lower pH value the solution will have more H⁺ ions that will compete with the metal cations in the solution for binding with the active sites. At pH values higher than 3, a considerable jump in the sorption capacity is observed to reach 70 % for lead at pH 5.5, 89% for copper at pH 6.0, and 44% for cadmium at pH 6.0. Further increase in the pH value lead to more increase in the % removal of the three metals, however this increment is basically being related to the precipitation of the metal ions, as the metals (Pb, Cu, Cd) tend to form insoluble M(OH)₂ form at higher pH. So that, the optimum pH values were revised to 5.5 for lead, and 6.0 for both copper and cadmium. The metal uptake capacity; q (mg metal/gram composite) at these pH values are 10, 13.3, 6.7 mg/g for lead, copper, and cadmium respectively. As the optimum pH of the three target metal is less than the pHzcp of the composite, the electrostatic interaction (physisorption) between the metal ions M⁺² and the surface of the composite could be hard, and other mechanism (chemisorption) could be work

as a dominant mechanism between M^{+2} ions and the active groups on the composite surface.

3.2.3. Effect of contact time

Figure 6 shows that the rate of metal sorption is rapid during the first 5 minutes to reach to 30%, 29 %, 21% for lead, copper, and cadmium respectively in the first 5 minutes. After then, the removal capacity of the composite increases slowly until reaches its breakthrough of its sorption capacity (qe) after approximately 240 minutes, at which the sorption capacity reaches to 12.2 mg/g with % removal of 81 % for lead, 13.1 mg/g with & removal of 87% for copper, and 10.4 mg/g with % removal of 69 % for cadmium. Generally, the fast sorption capacity at first 5 minutes could be attributed to physical sorption particularly with the effect of AC or /and the ion exchange with the elements in the composite (as shown in EDX analysis), and the slow rate at later stage attributed to chemical complexation with the active sites of the chitosan in the composite.

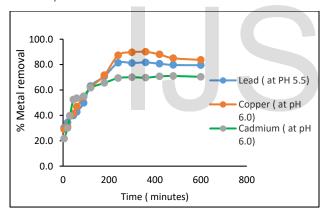


Figure 6: Effect of contact time on sorption of 30 mg/L heavy metals using 2g/L CH/AC composite - % removal.

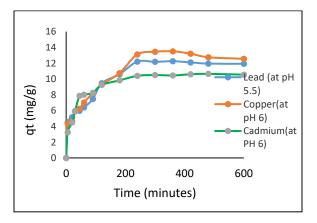


Figure 7: qt and qe of 30 mg/L heavy metals using 2g/L CH/AC composite.

3.2.4. Effect of sorbent dose

Figure 8 shows that, increasing of composite dose from [0.5 gm/L to 3 .0 gm/L in case of Pb, and Cd and to 2.5 gm/L in case of Cu], results in dramatically increase in the percentage uptake of the metals. After then, further increasing in the composite dose leads to decrease in the % uptake. However, the specific uptake; q (mg/g) shows reverse trend at the same time. This might be attributed to that the sorption system should have an equilibrium in the ratio of sorbent / sorbate.

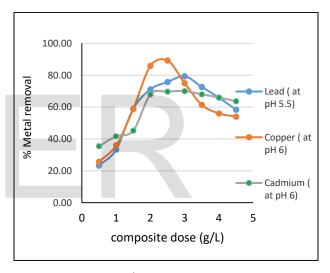


Figure 8: Effect of CH/AC composite dose on sorption of 30 mg/L heavy metals, for 4 hrs - % removal.

3.2.5. Effect of initial metal concentration

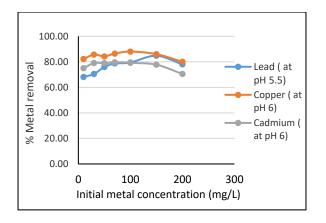


Figure 9: Effect of initial metal concentration on sorption of heavy metals, for 4 hrs - % removal.

Figure 9 shows that, percentage of metals uptake and the specific uptake; q (mg/g) increase by increasing the initial concentration of the metal to certain ratio in the system. After then, more increase in the metal concentration leads to decrease in the percentage uptake, however the specific uptake; q (mg/g) still increase. Decreasing in the percentage of metal uptake by increasing the metal concentration after certain ratio might be attributed to that, increasing of metal concentration result in establishing of completion between the metal ions to bind with the limited number of active sites on the sorbent.

3.3. Sorption isotherm models

3.3.1 Langmuir & Frendlich isotherm models

Application of adsorption isotherms indicated that the adsorption isotherm of (lead, copper, and cadmium) by the composite is correlated well with the Langmuir type. Which revealed the possibility of chemisorption mechanism as a dominant mechanism in this process. The small value of b in Langmuir model and the high value of 1/n in Freundlich model indicate that, the affinity or the bond strength between the metals and the active sites of the composite is weak which makes the desorption process easier.

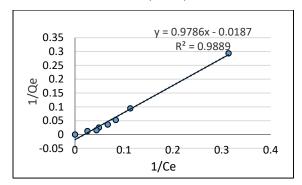


Figure 10: Langmuir isotherm model for sorption of Pb (II) by CH/AC composite at 22± 0.5 °C

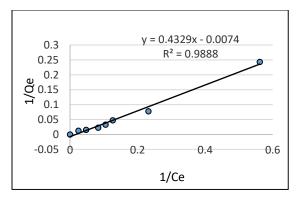


Figure 11: Langmuir isotherm model for sorption of Cu (II) by CH/AC composite at 22 ± 0.5 °C

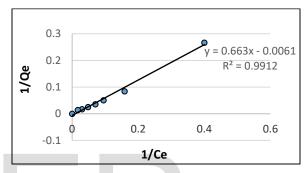


Figure 12: Langmuir isotherm model for sorption of Cd (II) by CH/AC composite at 22± 0.5 °C

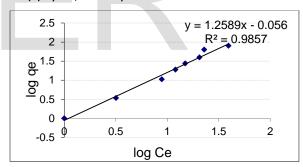


Figure 13: Freundlich isotherm model for sorption of Pb (II) by CH/AC composite at 22 ± 0.5 °C

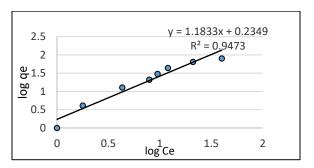


Figure 14: Freundlich isotherm model for sorption of Cu (II) by CH/AC composite at 22 ± 0.5 °C

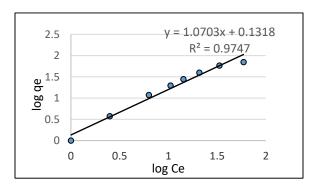


Figure 15: Freundlich isotherm model for sorption of Cd (II) by CH/AC composite at 22± 0.5 °C

Table 6.: Langmuir isotherm model parameters for sorption of Pb (II), Cu (II), and Cd (II) by CH/AC composite at $22\pm0.5\,^{\circ}\text{C}$

Metal	\mathbb{R}^2	b	Q max
Pb (II)	0.9889	0.019	53.47
Cu (II)	0.9888	0.017	135.1
Cd (II)	0.991	0.009	163

Table 7: Freundlich isotherm model parameters for sorption of Pb (II), Cu (II), and Cd (II) by CH/AC composite (at 22± 0.5 °C. C₀ 30.0 mg/L)

	-, -, -		
Metal	\mathbb{R}^2	1/n	K _F
Pb (II)	0.985	0.794	0.879
Cu (II)	0.947	0.84	1.71
Cd (II)	0.974	0.93	1.35

3.4. Sorption kinetic models

3.4.1. Pseudo 1st order& Pseudo 2st order kinetic

Results in **Tables 8 and 9** indicates that, the value of qe (experimental) does not agree with the qe (calculated) that was deduced from pseudo-first order model. This means that the applicability to employ pseudo-first order model in the sorption process of (Pb (II), Cu (II), and Cd (II)) onto CH/AC composite is infeasible. While, the value of qe (experimental) is quite closer to qe (calculated) that was deduced from pseudo-second order kinetic model. Also, the correlation coefficient (R²) in pseudo-second order model is close to the

unity. Hence, it can be concluded that, the adsorption of (Pb (II), Cu (II), and Cd (II) on CH/AC composite follow the pseudo-second order kinetic model. So, it can be considered that, the rate–limiting factor might be chemisorption involving valance forces through sharing of electrons between the amino groups of chitosan and the metal ions.

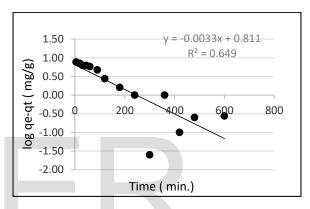


Figure 16: Pseudo first order kinetic plot of Pb (II) sorption by CH/AC composite (at 22 ± 0.5 °C, $C_0=30$ mg/L)

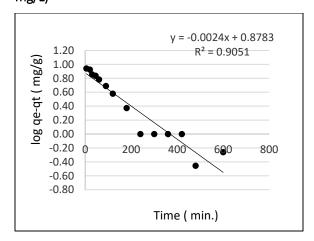


Figure 17: Pseudo 1st order kinetic plot of Cu (II) sorption by CH/AC composite (at 22 ± 0.5 °C, C₀= 30 mg/L

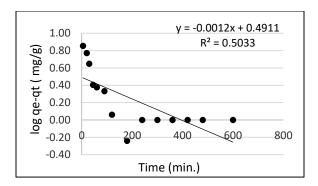


Figure 18: Pseudo first order kinetic plot of Cd (II) sorption by CH/AC composite (at 22 \pm 0.5 °C, C₀= 30 mg/L)

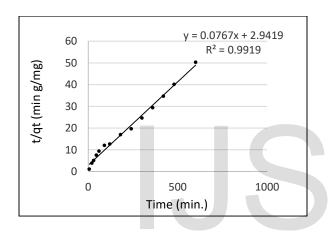


Figure 19: Pseudo 2^{nd} order kinetic plot of Pb (II) sorption by CH/AC composite (at 22 ± 0.5 °C, $C_0=30$ mg/L)

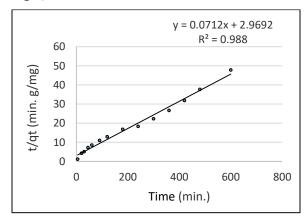


Figure 20: Pseudo second order kinetic plot of Cu (II) sorption by CH/AC composite (at 22 ± 0.5 °C, $C_0=30$ mg/L)

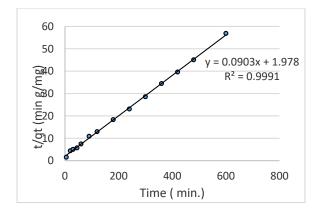


Figure 21: Pseudo second order kinetic plot of Cd(II) sorption by CH/AC composite (at 22 ± 0.5 °C, $C_0=30$ mg/L)

Table 8: Pseudo first order rate constants for sorption of Pb (II), Cu (II), and Cd (II) by CH/AC composite (at 22 ± 0.5 °C, $C_0 = 30.0$ mg/L)

Metal	Experimental	R ²	Calculated	K ₁ (min) ⁻¹
	qe (mg/g)		$q_e (mg/g)$	
Pb (II)	12.2	0.6	6.47	0.007
Cu (II)	13.1	0.9	7.55	0.005
Cd (II)	10.4	0.5	3.098	0.002

Table 9: Pseudo 2nd order rate constants for sorption of Pb (II), Cu (II), and Cd (II) by CH/AC composite (at 22 ± 0.5 °C, $C_0 = 30.0$ mg/L)

Metal	Expermintal qe (mg/g)	\mathbb{R}^2	Calculated q _e (mg/g)	K ₂ (g/mg min)
Pb (II)	12.2	0.9919	13.03	0.002
Cu (II)	13.1	0.988	14.04	0.002
Cd (II)	10.4	0.9991	11.07	0.004

3.5. Conclusion

Chitosan/Activated carbon composite represents a promise eco-friendly biopolymer material, as:

• Its moderate bulk density makes it a suitable polymeric material for using in the industrial wastewater treatment plants.

- •It has significant removal efficiency for the common toxic heavy metals in the wastewater; (Pb. Cu. Cd).
- It can be successfully used as effective, low cost sorbent material and as alternative to costlier sorbent polymers.
- It gives a highest removal efficiency at pH close to the pH of the wastewater (5.5 for lead and 6.0 for Copper and cadmium), which reduce the need for chemical addition
- The sorption process of the three metals was fitted well with Langmuir isotherm model and pseudo second order kinetic model
- Chemisorption by chelation via making coordinate bond between the free electron pairs (of the nitrogen of the amine group, as well as the oxygen of the hydroxyl group) in chitosan and the void orbital of the metal cations is the dominant mechanism.
- •However, the physical adsorption and ion exchange are possible mechanisms by small participation.
- Presence of activated carbon improve the chitosan activity by increasing its surface area.

5.References

- [1] T.A.H. Nguyen, H.H. Ngo, W.S. Guo, J. Zhang, S. Liang, Q.Y. Yue, Q, Li, T.V. Nguyen (2013). Applicability of agricultural waste and by-products for adsorptive removal of heavy metals from wastewater. Bioresource Technology, 148, pp 574-585, (2013).
- [2] Othman, Za, Hashim, M., and Habila, Ma. (2011) "Kinetic, equilibrium and thermodynamic studies of cadmium (II) adsorption by modifies agricultural wastes" Molecules 16 (12): 10443-10456
- [3] Fenglian Fu, Qi Wang. (2011). Removal of heavy metal ions from wastewaters: A review. Journal of environmental management. 92 407-418.
- [4] Kupper, T., D. Burge, H.J. Bachmann, S.Gusewell, and J. Mayer (2014) "Heavy metals in source-separated compost and digestates" Waste Management 34: 867-874
- [5] Lenntech, Heavy metals http:// lenntech.com/heavymetals.htm (12 December 2013)
- [6] Mohsen Arbab, Sara Hemati, Masoud Amiri. (2015). Removal of lead ions from industrial

- wastewater: A review of removal methods. International journal of epidemiologic research. 2: 105-109.
- [7] M. Soundarrajan, T. Gomathi, P.N. Sudha. (2013). Understanding the adsorption efficiency of chitosan coated carbon on heavy metal removal. International journal of scientific and research publications. 2250-3153.
- [8] Jianlong Wang, Can Chen. (2014). Chitosan-based biosorbents: Modification and application for biosorption of heavy metals and radionuclides. Journal of bioresource technology 160: 129-141.
- [9] World Health Organization (2011). Guidelines for drinking water quality, fourth edition (2011). https://www.who.int/water sanitation health/publications/drinking-water-quality-guidelines-4-including-1st-addendum/en/
- [10] Coulibaly Lacina, G. Germain, and A.N. Spiros. (2003). Utilization of fungi for biotretment of raw wastewater. African Journal of Biotechnology. Vol. 2, No. 12, pp. 620-630.
- [11] M. Gavrilescu. (2004). Removal of heavy metals from the environment by Biosorption. Engineering in Life Sciences. Vol. 4, No. 3, pp. 219-232
- [12] T.A.H. Nguyen, H.H. Ngo, W.S. Guo, J. Zhang, S. Liang, Q.Y. Yue, Q, Li, T.V. Nguyen (2013). Applicability of agricultural waste and by-products for adsorptive removal of heavy metals from wastewater. Bioresource Technology, 148, pp 574-585, (2013).
- [13] Natalya, T.V.Ramachandra, and R.D.Kanamadi. (2003). Biosorption of heavy metals. Research Journal of Chemistry and Environment.Vol. 7, No. 4, pp.71-79
- [14] Rani Gupta, P. Ahuja, S.Khan, R.K.Saxena, and H.Mohapatra., (2000). Microbial Biosorbents: Meeting Challenges of Heavy metal
- [15] Józef Synowiecki, and Nadia Ali Al-Khateeb (2003). Critical review in food science and nutrition, 43 (2): 145-171 (2003).
- [16] Rayane Santa Cruz Martins, and Bianca Rosa Paschoal (2017). Preparation and characterization of chitosan obtained from shells of shrimp (*Litopenaeus vannamei* boone). Journal of marine drugs, (2017), 15,141.
- [17] Christian Schmitz, Lilian González Auza, David Koberidze, Stefan Rasche, Rainer Fischer,

- and Luisa Bortesi (2019). Conversion of Chitin to Defined Chitosan Oligomers: Current Status and Future Prospects. Journal of Marine Drugs, 17, 452; (2019).
- [18] Marguerite Rinaudo (2006). Chitin and chitosan: properties and applications. Journal of Progress in polymer science, (2006), volume 31, issue 7, pp 603-632.
- [19] W.S. Wan Nagah, A. Kamari, and Y. J. Koay (2004). Equilibrium and kinetics studied of adsorption of copper (II) on chitosan and chitosan /PVA beads. International journal of biological macromolecules, vol.34: 155-0161.
- [20] Jianlong Wang, and Can Chen. (2014). Chitosan- based biosorbents: Modification and application biosorption of heavy metals and radionuclides. *Journal of bioresource technology* 160: 129-141, 2014.
- [21] Ashfaq Ahmad, Hassan Mohammed Al-Swaidan* and Ahmad Hamed Alghamdi (2015). Production of Activated Carbon from Raw Date Palm Fronds by ZnCl2 Activation. J.Chem.Soc.Pak. Vol.37, No. 06, 2013.
- [22] Hakimeh Sharfifard, Farzin Zokaee Ashtiani, Mansooreh Soleimani. (2012). Adsorption of palladium and platinum from aqueous solutions by chitosan and activated carbon coated with chitosan. Asia-Pacific Journal of chemical engineering, vol. 8, pp:384-395, 2012.
- [23] Viorica Patrulea, Anamaria Negrulescu, Manuela M. Mincea, Laura D. Pitulice, Otilia Bizerea Spiridon, and Vasile Ostafea,(2013). Optimization of the Removal of Copper(II) Ions from Aqueous Solution on Chitosan and Cross-Linked Chitosan Beads. Journal of bioresources 8 (1), 1147-1165; 2013.
- [24] Xiaoyu Chen and Lindun He, (2017). Microwave irradiation assisted preparation of chitosan composite microsphere for dye adsorption. International journal of polymer science, volume 2017, article ID 2672597, 8 pages; 2017.
- [25] H.Sharififard, M.Nabavinia, M.Soleimani (2016). Evaluation of adsorption efficiency of activated carbon/chitosan composite for removal of Cr (VI) and Cd (II) from single and bi-solute dilute solution. Advanced in environmental technology 4,2016.

- [26] Elisee Nsimba Bakatula, Dominique Richard, Carmen Mihaela Neculita and Gerald J. Zagury (2018). Determination of point of zero charge of natural organic materials. Journal of Environmental Science and Pollution Research, 25, pp:7823–7833, 2018.
- [27] W.S. Wan Ngah, L.C.Teong, R.H.Toh, M.A.K.M. Hanafiah, (2012). Utilization of chitosan-zeolite composite in the removal of Cu (II) from aqueous solution: Adsorption, desorption, and fixed bed column studies. Chemical engineering journal, 209(2012),
- [28] Jude C. Igwe, Augustin A. Abia, 2007. Equilibrium sorption isotherm studies of Cd(II), Pb(II) and Zn(II) ions detoxification from waste water using unmodified and EDTA-modified maize husk. Electronic Journal of Biotechnology, Vol. 10 No. 4, Issue
- [29] Rodriguez CE, Quesada A, Rodriguez E (2006) Nickel biosorption by Acinetobacter baumannii and Pseudomonas aeruginosa isolated from industrial wastewater. Brazil Journal of microbiology 37:465–467, 2006.
- [30] Sarma , P, Kumar, R. & Pakshirajan, K. 2015 Batch and continuous removal of copper and lead from aqueous solution using cheaply available agriculture waste materials. International Journal of Environmental Research 9 (2),635-648
- [31] Mambo Moyo, Linda Chikazaza, Benias Chomunorwa Nyamunda, and Upenyu Guyo (2013). Adsorption batch studies on the removal of Pb (II) using Maiz Tassel based activated carbon. Vol. 2013, article ID 508934, 8 pages.
- [32] Qiqi Ding and Xijun Hu (2019). Mesoporous Materials as Catalyst support for WastewaterTreatment.Madridge.Journal of Nanotechnology & Nanoscience. June 18, 2019, ISSN: 2638-2075.
- [33] Asha H. Gedam and Rajendra S. Dongre (2015). Adsorption characterization of Pb (II) ions onto iodate doped chitosan composite: equilibrium and kinetic studies. Journal of royal society of chemistry (RSC Advances), 5: 54188-54201, 2015.
- [34] Venkatesham, V., G.M.Madhu, S.V. Satyanarayana, and H.S.Preetham (2013) "Adsorption of lead on gel combustion derived

nano ZnO" Procedia Engineering, 51: 308-313, 2013.

[35] Cechinel, M.A., S.M. Souza, and A.A. Souza (2014) "Study of lead (II) adsorption onto activated carbon originating from cow bone" Journal of Cleaner Production 65: 342-349. 2014.

[36] Pitsari, S.,E., Tsoufakis, and M.Loizidoi, (2013). Enhanced lead adsorption by unbleached newspaper pulp modified with citric acid. Chemical Eng. journal, 223, 18-30,2013.

IJSER